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# An Alternative Method for Estimating the Phase Fraction of Multiphase Nanomaterials: Analysis from X-ray Diffraction

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## ABSTRACT

The presence of multiple phases/ components within a nanocomposite material impacts its properties. Therefore, there is a need to estimate the phase fraction of each element present in a sample. Spurr-Myers proposed a valuable formula for calculating the rutile and anatase phase fraction of a TiO<sub>2</sub> sample from X-ray diffraction. However, this formula is dedicated to TiO<sub>2</sub> and is inapplicable to samples that contain more than two phases. The present research proposed a simple method for quantifying the phase fraction of all types of nanomaterials consisting of two or more phases. The precision/ accuracy test, conducted by multiplying the total intensity of all the diffraction peaks present in a sample with the value of the phase fraction of individual components, showed that the proposed method gave precision values equivalent to the sum of the intensity of the peaks for each element. Meanwhile, the S-M gave precision values that were significantly inconsistent with the sum of the intensity of the peaks of each component. The study showed that the proposed method was valid for a wide range of  $2\theta$  values and can be deployed to obtain reasonable and reliable values of phase fraction that could assist in understanding the material phase fractionproperties relationship.

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## 1. Introduction

A nanocomposite material is a mixture of different nanomaterials (materials with at least one of its dimensions falling in the nanometer scale range of (1-100 nm). In other words, a nanocomposite is a multiphase solid nanomaterial (in the form of nanoparticles or thin film) in which one of the components has one, two, or three dimensions  $\leq 100$  nm. A nanocomposite retains the unique characteristics of each component. Nanocomposites

offer excellent material properties that may be difficult to achieve from the individual component [1] and lead to the enhancement of device performance due to the synergistic effect between the components/ phases [2-6]. One of the interesting characteristics of a nanocomposite is the formation of a heterojunction (which aids charge carrier separation and transport) at the interface between the phases [6-8]. Nanocomposites such as ZnO/Ga<sub>2</sub>O<sub>3</sub>, α- $Fe_2O_3/CuO$ ,  $Ga_2O_3/GaN$ ,  $MoO_3/TiO_2/Ti_3C_2T_x$ , and  $Ga_2O_3/TiO_2$  have been produced and applied for photoelectrochemical water splitting, photodetection, chemical sensing, and biological treatment against bacterial [6-10]. A nanocomposite material is a mixture of different nanomaterials (materials with at least one of its dimensions falling in the nanometer scale range of (1-100 nm). In other words, a nanocomposite is a multiphase solid nanomaterial (in the form of nanoparticles or thin film) in which one of the components has one, two, or three dimensions  $\leq 100$  nm. A nanocomposite retains the unique characteristics of each component. Nanocomposites offer excellent material properties that may be difficult to achieve from the individual component [1] and lead to the enhancement of device performance due to the synergistic effect between the components/ phases [2-6]. One of the interesting characteristics of a nanocomposite is the formation of a heterojunction (which aids charge carrier separation and transport) at the interface between the phases [6-8]. Nanocomposites such as ZnO/Ga<sub>2</sub>O<sub>3</sub>, α-Fe<sub>2</sub>O<sub>3</sub>/CuO, Ga<sub>2</sub>O<sub>3</sub>/GaN, MoO<sub>3</sub>/TiO<sub>2</sub>/Ti<sub>3</sub>C<sub>2</sub>T<sub>x</sub>, and Ga<sub>2</sub>O<sub>3</sub>/TiO<sub>2</sub> have been produced and applied for photoelectrochemical water splitting, photodetection, chemical sensing, and biological treatment against bacterial [6-10]. Because of their improved material characteristics due to the heterojunction formation and synergetic effect between the phases, it is desirable to quantify how much a component is present in a synthesised sample. Many measurement techniques have been employed to calculate the phase fraction (P.F.) in solid nanomaterial, including electron backscatter diffraction [16, 17], energy dispersive synchrotron X-ray diffraction [18], neutron diffraction [19], and X-ray diffraction (XRD) analysis [2, 20-23]. The P.F. of the components present in a sample can be calculated from experimental data derived from the various measurement techniques. The Rietveld refinement was the first general method that was proposed for P.F. analysis. The method was published in 1967 [24]. The Rietveld method can be applied to all natural and synthetic materials. It can be performed on multiphase crystalline and amorphous materials [25]. The Rietveld method is a full-profile fitting technique that considers the entire diffraction pattern of a sample for quantitative P.F. analysis [26, 27]. This makes the method more reliable than traditional methods that utilise a small, pre-selected set of integrated intensities. The wide acceptability of the Rietveld method for quantitative phase analysis is evident in the many publications on different classes of materials [26, 28–31]. Several researchers do not use the Rietveld method despite its high accuracy and widespread acceptability, probably because the idea is unclear. The authors who have applied this method do not present the simplified step-by-step approach to using the Rietveld method to calculate the P.F. in a sample [25–27, 29]. Therefore, there is a need to develop simpler or easier-to-understand methods for P.F. analysis. The method proposed by Spurr and Myers (S-M) in 1957, about a decade before Rietveld's method, was the first quantitative approach for estimating the P.F. of the various components present in a sample. The method was proposed for estimating the P.F. of rutile and anatase from the XRD data of TiO<sub>2</sub> nanomaterials [21]. The S-M formula (Eq. (1) and (2)) has remained the most typical method for quantifying the P.F. of  $TiO_2$  samples for decades.

$$f_A(\%) = \frac{0.79I_A}{I_R + 0.79I_A} \times 100$$
(1)  
$$f_R(\%) = (1 - f_A) \times 100$$
(2)

where 
$$f_A$$
 Is the P.F. of anatase,  $f_R$  Is the P.F. of rutile,  $I_A$  is the strongest intensity of anatase and  $I_R$  is the strongest intensity of rutile. Unlike the Rietveld method, the S-M relation is an averaging method that considers only the strongest/ predominant diffraction peaks of the rutile and anatase phases present on the XRD pattern of a TiO<sub>2</sub>

intensity of rutile. Unlike the Rietveld method, the S-M relation is an averaging method that considers only the strongest/ predominant diffraction peaks of the rutile and anatase phases present on the XRD pattern of a  $TiO_2$  sample. Aside from being dedicated to the  $TiO_2$  material, the S-M relation is valid for a bi-phase  $TiO_2$  sample only and cannot be deployed for a  $TiO_2$  sample consisting of more than two phases.

Another widely used method for determining P.F. considers the relative intensity ratio of the characteristic peaks of the phases present in a sample (Eq. (3) and (4)) [32-35]. Just like the S-M method, the relative intensity ratio method considers only the predominant diffraction peak per component. It does not use all the peaks present in a diffraction pattern. However, its advantage over the S-M method is that it can be applied to a sample of two or more phases [32, 33]. The limitation of the two methods is that they consider only the intensities of the strongest

diffraction peaks, thereby giving P.F. values that are not accurate. Overall, the Rietveld method is superior to the other two methods because it provides a more precise result by fitting the entire diffraction pattern of a sample.

$$f_B = \frac{I_B}{I_B + I_C + I_D \pm \cdots} \times 100\%$$
(3)

$$f_C = \frac{I_C}{I_B + I_C + I_D \pm \cdots} \times 100\%$$
(4)

where  $f_B$  Is the P.F. of phase B,  $f_C$  Is the P.F. of phase C,  $I_B$  is the strongest intensity of component B and  $I_C$  is the predominant intensity of component C. The P.F. of component D can be calculated in a similar manner, and so on [32-35]. An inference from the preceding paragraphs shows that there is a need to propose a simple but general method that can be used to estimate the P.F. of a multiphase nanomaterial. Unlike the S-M and relativeintensity-ratio methods, the proposed method should consider all the diffraction peaks to get an accurate estimate of the P.F. of the components in a sample. The proposed method should apply to all nanomaterials, like the Rietveld method. The present work proposes a typical method for estimating the P.F. of all kinds of nanocomposite materials with two or more phases. Unlike the S-M, the proposed method is general, which can only be applied to a bi-phase TiO<sub>2</sub> sample and cannot be used for other multiphase nanomaterials.

## 2. Experimental Procedure

## 2.1 Sample Preparation

 $Ga_2O_3/ZnO$  nanocomposite and  $TiO_2$  films were used for this study. The  $TiO_2$  film was synthesised by anodisation and post-annealed at 450 °C as described in our previous report [20]. Before synthesis, a 0.127-mm thick Ti foil (purity 99.7%) was cut into a small piece of size  $1 \times 1$  cm<sup>2</sup>. The Ti foil substrate was washed by sonicating it in methanol and acetone for 20 minutes, followed by bathing it with deionised water, and then subsequently drying it in an oven. Anodisation was carried out in a Teflon cubicle consisting of the Ti foil substrate as the anode and a platinum bar as the counter electrode connected to a Keithley model-2400 as the voltage source. An electrolyte prepared by mixing 0.1 wt% NH<sub>4</sub>F, 2 wt%  $H_2O$ , and 98 wt% ethylene glycol was deployed for the reaction. A two-step anodisation process was employed to synthesise at room temperature under a direct current voltage for 2 h. The prepared TiO<sub>2</sub> layer was mechanically detached after the first-step anodisation. The second-step anodisation involved a repetition of the first-step synthesis. The fabricated film was immediately washed with deionised water and dried in the oven. The prepared film was annealed in a horizontal tube furnace at 550 °C under a water vapour/  $N_2$  supply for 3 h. The water vapour was supplied as an oxygen source for the oxidation of the film. On the other hand, the  $N_2$  gas was used as a carrier gas to supply the vapour into the reactor [20]. On the other hand, a two-step growth technique was used to prepare the  $Ga_2O_3/ZnO$  nanocomposite film. This was to ensure the solubility of ZnO and Ga<sub>2</sub>O<sub>3</sub> in the gas phase to obtain a nanocomposite having prominent diffraction peaks of Ga<sub>2</sub>O<sub>3</sub> and ZnO. Firstly, about 50 mg Ga<sub>2</sub>O<sub>3</sub> powder (99.998% purity, Strem Chemical Inc.) was placed in a partially covered ceramic boat and loaded to the center/ hot zone of a horizontal tube chemical vapour deposition (CVD) system for decomposition at 950 °C. The reactor supplied 100 sccm  $H_2$  reducing gas to aid thermal decomposition for 60 min (where sccm is cubic centimeter per minute). The furnace was shut down, and a coating could be seen on the inner walls of the boat. In the second step, 30 mg of ZnO powder (99.99% purity, Kock-Light Laboratories Ltd) was mechanically mixed with 10 mg Ga<sub>2</sub>O<sub>3</sub>, placed in the Ga<sub>2</sub>O<sub>3</sub>-contaminated boat, and transferred to the center zone of the CVD. Si(111) substrate of size  $1 \times 1$  cm<sup>2</sup> was placed vertically on support and loaded downstream of the furnace at a separation of 24 cm from the precursor. The temperature of the furnace was raised from room temperature to 950 °C, while flowing 100 and 600 sccm  $H_2$  reducing gas and  $N_2$  carrier gas, respectively, into the horizontal reactor. The deposition was sustained for 60 min before the furnace was shut down. A coating could be seen on the substrate [36, 37].

#### 2.2 Characterisation

The prepared TiO<sub>2</sub> and Ga<sub>2</sub>O<sub>3</sub>/ZnO films were characterised using a PANalytical X'pert PRO MRD PW3040 highresolution X-ray diffractometer (XRD) employing Cu-K $\alpha$  ( $\lambda = 0.15406$  nm) radiation. The XRD was operated at room temperature under a generator setting of 40 mA and 40 kV. The samples were scanned between the Bragg-Brentano geometry ( $\theta$ -2 $\theta$ ) of 20–75° at the step size of 0.05° and scan time of 1.5 s. The divergence slit size of 0.2393°, receiving slit size of 0.1 mm, a focus-divergence distance of 91 mm, and a goniometer radius of 320 mm were deployed for optimum measurements [13]. Phase identification was carried out using a HighScore software attached to the XRD. The software matched the diffraction peaks with the database (Joint Committee on Powder Diffraction Standards (J.C.P.D.S.)).

#### 2.3 The proposed Method for P.F. Analysis of a Multiphase Nanomaterial

Unlike the S-M relation, the proposed method is a holistic approach that considers the intensities of all the prominent diffraction peaks on a measured sample. The proposed method for the P.F. analysis of multiphase nanomaterials makes the following assumptions: (i) The sum of the intensity of the diffraction peaks of a particular component/ phase is directly proportional to the weight/ density of this component contained on the measured sample [21, 38], according to Eq. (5). (ii) The sum of the intensity of all the diffraction peaks on a sample (irrespective of the component/ phase) is directly proportional to the overall weight of the nanomaterial contained in the sample (Eq. (6)). (ii). The sum of the estimated P.F. of the various components found in a sample should be equal to 100 since P.F. can be expressed in percentage.

$$I_{sx} = K_1 w_x \tag{5}$$

$$I_{gt} = K_2 w_0 \tag{6}$$

where  $I_{sx}$  Is the sum of the intensity of all diffraction peaks belonging to a particular component x,  $w_x$  is the weight of component x contained in the sample,  $I_{gt}$  Is the grand/ overall total of the intensity of all diffraction peaks contained in the sample,  $w_o$  Is the overall weight of the nanomaterial on the sample being measured and  $K_1 = K_2$ is a constant equal to unity for the materials contained on the same measured sample [21, 38]. Dividing Eq. (5) by Eq. (6) yields,

$$\frac{K_1}{K_2} \cdot \frac{w_x}{w_o} = \frac{I_{sx}}{I_{gt}}$$

where  $\frac{w_x}{w_o} = f_x$  is the phase/ weight fraction of a particular component x.

Expressing Eq. (7) in percentage leads to Eq. (8):

$$f_x(\%) = \frac{I_{sx}}{I_{gt}} \tag{7}$$

$$f_x(\%) = \frac{I_{sx}}{I_{gt}} \times 100 \tag{8}$$

Eq. (8) can be employed to estimate the P.F. of all nanomaterials. Although S-M has derived a dedicated relationship for the P.F. analysis of  $TiO_2$ , Eq. (6) can alternatively be applied for the  $TiO_2$  to estimate the P.F.s of rutile and anatase contained in a  $TiO_2$  sample. It should be noted that the proposed method can be used for a nanocomposite having more than two phases, unlike the S-M method.

#### **3. Experimental Procedure**

Fig. 1 shows XRD patterns of the synthesised TiO<sub>2</sub> film and Ga<sub>2</sub>O<sub>3</sub>/ZnO nanocomposite. The XRD pattern of TiO<sub>2</sub> (Fig. 1a) exhibits diffraction peaks belonging to anatase with the prefix A and rutile with the prefix R, according to the Joint Committee on Powder Diffraction Standards (J.C.P.D.S.) card nos. 01-071-1167 and 01-077-0442, respectively. The anatase TiO<sub>2</sub> peaks were more intense, indicating its dominance in the sample. The metallic titanium (Ti) peaks marked with the prefix T (according to J.C.P.D.S. card no. 01-089-2782) were reflections from the Ti foil substrate used for the TiO<sub>2</sub> synthesis. The strongest/ predominant crystallographic peaks for anatase and rutile were the A(101) and the R(004) planes, respectively. Meanwhile, the dominance of the anatase over rutile at the post-annealing temperature of 450 °C was consistent with the literature [11, 20, 39]. Fig. 1a reveals the surface micrograph of the anodised TiO<sub>2</sub> film, as contained in the Supporting Document. Meanwhile, Table 1 presents the elemental composition of the samples.



Figure 1: XRD patterns of the (a) anodised TiO<sub>2</sub> film (b) CVD-grown Ga<sub>2</sub>O<sub>3</sub>/ZnO nanocomposite.

The XRD pattern for the nanocomposite (Fig. 1b) evinced crystallographic reflections belonging to the monoclinic phase of Ga<sub>2</sub>O<sub>3</sub> ( $\beta$ - Ga<sub>2</sub>O<sub>3</sub>), which is marked with the prefix G and hexagonal ZnO marked with the prefix Z, according to J.C.P.D.S. card nos. 00-043-1012 and 01-074-0534, respectively. ZnO peak intensities were relatively low compared to the  $\beta$ - Ga<sub>2</sub>O<sub>3</sub> peaks due to the smaller amount of the ZnO material in the sample [7] (Table 1). Fig. 1b shows the surface morphology of the CVD-grown Ga<sub>2</sub>O<sub>3</sub>/ZnO film. Peak profile analyses were carried out using the S-M relation, and the proposed method for determining P.F. is presented in Table 1. According to the S-M method, the intensity  $I_{A}$  of the strongest anatase peak (A(101)) and the intensity  $I_{R}$  of the strongest rutile peak (R(004)) were used to calculate the P.F. of anatase ( $f_A$ ) and rutile ( $f_R$ ), respectively (Fig. 1, pattern a). The values of  $I_{A}$  and  $I_{R}$  were substituted into the S-M formula (Eq. 1), and the resulting value of  $f_A$  was substituted into Eq. 2 to find  $f_R$  for the b-phase TiO<sub>2</sub> film. The proposed method (Eq. 8) was applied for the P.F. analysis of the biphase TiO<sub>2</sub> sample to check if it could provide values equivalent to those obtained from the TiO<sub>2</sub>-dedicated S-M method (Table 1).

Sample	Material phase	I <sub>sx</sub>	$I_{gt}$	P.F. (%) by the S- M method	P.F. (%) by the PM -	<b>Precision check</b> = $I_{gt} \times PF$	
						S-M	PM
TiO <sub>2</sub>	Anatase	235.67	288.71	74.40	81.63	214.80	235.59
	Rutile	53.04		25.60	18.37	73.91	53.12
GO/ZO	β-Ga <sub>2</sub> O <sub>3</sub>	734.06	1112.51	63.93	65.98	711.23	734.03
	ZnO	378.45		36.07	34.02	401.28	378.48

Table 1: Peak profile analysis of the various components on the TiO<sub>2</sub> and Ga<sub>2</sub>O<sub>3</sub>/ZnO films.

Notes: - GO/ZO: Ga<sub>2</sub>O<sub>3</sub> /ZnO, PM: proposed method.

It was evident that the sum of the anatase and rutile peak intensities were 235.67 and 53.04, respectively, giving a grant total intensity of 288.71 for the TiO<sub>2</sub> sample. Meanwhile, the P.F. of anatase and rutile were calculated from the S-M method and found to be 74.4 and 25.6%, respectively. On the other hand, the proposed method gave P.F. values of 81.6 and 18.4% for anatase and rutile, respectively. This indicates a significant difference in the magnitude of the values of the P.F.s estimated from the two methods, which suggests that the proposed method may not be suitable for the TiO<sub>2</sub> material. Nevertheless, the precision/ success check showed that the proposed method could be ideal for the P.F. analysis of TiO<sub>2</sub> because it yielded ( $I_{gt} \times P.F.$ ) values that were equivalent to

the sum of the intensity of the diffraction peaks for a particular component  $I_{sx}$  measured directly from the XRD pattern. Meanwhile, the ( $I_{gt} \times P.F.$ ) values obtained from the S-M method varied significantly from the observed  $I_{sx}$  for anatase and rutile, which were measured directly from the XRD pattern. This suggests that the S-M is not infallible/ perfect, indicating that the proposed method can be an alternative to P.F. analysis. It should be noted that the sum of the XRD intensities from a particular component, x, is proportional to the amount of this material found in the measured sample. In other words, the component/ phase with a small or large amount on a sample will produce weak or strong diffraction peaks, respectively, from the XRD measurement [40-43]. The component with the highest amount of P.F. on a sample would produce the strongest diffraction peaks. Peak profile analysis of the Ga<sub>2</sub>O<sub>3</sub>/ZnO film using the proposed method gave P.F. values of 65.98 and 34.02% for the Ga<sub>2</sub>O<sub>3</sub> and ZnO components, respectively. Precision check given  $(I_{at} \times P.F.)$  values that were equivalent to the sum of the intensity of the diffraction peaks for a component  $I_{sx}$  measured directly from the XRD pattern. This also validates the proposed method for P.F. analysis. To confirm if the estimated values for the P.F. of the Ga<sub>2</sub>O<sub>3</sub> and ZnO components were reasonable, the S-M was applied to the  $Ga_2O_3/ZnO$  film. Estimates show that the P.F. of  $Ga_2O_3$ and ZnO was 63.93 and 36.07%, respectively. A comparison shows that the values of the P.F. for  $Ga_2O_3$  and ZnO derived from the two methods vary slightly by a magnitude of 2.05. This suggests that the proposed method is reasonable. More interestingly, it can be applied to samples with more than two phases. It is necessary to state that the scale of the  $2\theta$  axis must be kept between a wide range (to read all diffraction peaks) for the proposed method to yield a reasonable/ proper P.F. value. This is because the present method considers (sums up) all the prominent peaks in a sample, unlike the S-M relation, which considers only the intensity of the strongest peak per component.

## 4. Conclusions

In summary, the present paper proposed a method for estimating the P.F. of a multiphase nanomaterial from XRD data. The Spurr-Myers method was employed to check the appropriateness of this proposed method for P.F. analysis. XRD data of anodised  $TiO_2$  film and chemical vapour deposited  $Ga_2O_3/ZnO$  nanocomposite were used for this study. The proposed method was valid for a wide range of 2theta values and yielded reasonable P.F. values compared to those obtained from the Spurr-Myers method. Interestingly, the precision check showed that the estimated P.F. values obtained from the proposed method were more reasonable than those obtained from the Spurr-Myers method dedicated to  $TiO_2$  and limited to a bi-phase sample, the proposed method can be applied to all nanomaterials consisting of two or more phases to give a reasonable idea about the P.F. of all components present on a sample.

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## **Conflict of Interest**

The authors declare that they have no conflict of interest.

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